Research Article

Optimizing Operating Conditions for Oxidative Coupling Methane (OCM) in the Presence of NaCl-MnOx/SiO2

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Abstract
A novel NaCl-MnOx/SiO2, synthesized using slurry mixed method, was used as a catalyst in oxidative coupling of methane process. Optimal conditions were determined using both computational and experimental methods. NaCl, MnOx and SiO2 which are the component of our catalyst are studied. In this research, the catalyst provided the best experimental result when the ratio of MnOx to SiO2 was 2 to 1. CH4 conversion, C2+ selectivity, C2+ yield and C2H4/C2H6 ratio were achieved at 38%, 71%, 27% and 7.2, respectively when operated the process at optimal temperature of 750°C under atmospheric pressure with ratio of CH4:O2 at 4 and 3000 mL g^{-1} h^{-1} of weight hourly space velocity (WHSV). The catalytic performance of NaCl-MnOx/SiO2, was found to be higher than other recently developed catalysts. Besides, NaCl-MnOx/SiO2 gave only less than 10% selectivity of the unwanted CO2, while the other SiO2-based catalysts reported as high as 17% of CO2 selectivity. It also achieved high ethylene production when benchmark with previous research. The experimental results were validated using Aspen Plus at temperature ranging from 700 to 850°C.

Keywords: Oxidative coupling of methane (OCM), Ethylene production, Methane conversion, Novel catalyst

1 Introduction

Ethylene, a well-known key building block in petrochemical industry, can be utilized to many valuable chemicals i.e. polyethylene, ethylene dichloride, ethyl benzene, and vinyl acetate which are widely usage [1]–[4]. Ethylene is conventionally produced via cracking process of natural gas/crude oil which plays a major role for productions of highly valuable products from lower value of raw materials [5], although the process is reliable on fossil fuels, high energy consumption and releases large quantity of carbon dioxide (CO2)
[6]. Oxidative coupling of methane (OCM) is an alternative method to produce olefins from methane and oxygen. It advantages include 1) being independent from fossil fuels as it can utilize methane from alternative resources such as shale gas, synthetic methane from methanation process or methane-rich biogas 2) flexibility in using oxygen-based greenhouse gases as oxygen source, i.e. CO2 or N2O, instead of pure oxygen or air, and 3) more environmentally friendly as it could release zero carbon emission [7]. OCM consists of 2 main reactions, shown as Equations (1) and (2) [7].

$$2CH_4 + 0.5O_2 \leftrightarrow C_2H_6 + H_2O \ \Delta H_{298}^{o} = -177 \, kJ/mol \quad (1)$$

$$C_2H_4 + 0.5O_2 \leftrightarrow C_2H_4 + H_2O \ \Delta H_{298}^{o} = -105 \, kJ/mol \quad (2)$$

Oxygen concentration must be limited as it can shift the reaction towards complete combustion [Equation (3)] and partial oxidation process [Equation (4)] instead, giving CO_2 and CO as unwanted by-products, respectively [8].

$$CH_4 + 2O_2 \leftrightarrow CO_2 + 2H_2O \ \ \Delta H_{298}^{o} = -802 \, kJ/mol \quad (3)$$

$$CH_4 + 1.5O_2 \leftrightarrow CO + 2H_2O \ \Delta H_{298}^{o} = -519 \, kJ/mol \quad (4)$$
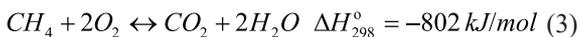
Low methane conversion (~20–30%) and low ethylene selectivity (~20–30%) had been reported as the main challenge of the OCM process when using the latest developed catalyst systems such as alkali-chloride based metal oxides [9]–[11]. A promising method that can be applied to resolve the above drawbacks is the design of effective catalyst properties, including catalyst compositions and/or surface textural, together with optimizing operating conditions [12], [13]. Amongst the recently developed catalysts, manganese oxides were reported to have the highest catalytic performance towards OCM due to its high electrical conductivity [14]. For example, by using an alkali chloride-promoted manganese oxide catalysts, NaCl/Mn oxide, 25.7% ethylene yield can be produced at 750°C [10]. SiO_2 has been used as support material. Calcination condition of SiO_2 showed the effect to phase and structure of the material [15]. Amorphous silica can yield active but very unselective catalysts whereas crystalline SiO_2 can active and highly selective catalysts with respect to the formation of ethylene and Na is a promoter in term of both structural and chemical side [16]. Highly crystallite α-cristobalite SiO_2 was proven to be highly selective for ethylene production whereas Na was found to be a beneficial alkali when used as structural and chemical promoter [14]–[17]. Preparing Na_2WO_4–Mn/SiO_2 catalysts by different methods can transformed α-cristobalite into highly crystallite α-cristobalite [18], A promising of Mn_2O_3–Na_2WO_4/SiO_2 catalyst showed the highest ethylene yield of 12.9% and ratio of ethylene and ethane at 1.3 can be achieved at 750°C, CH_4/O_2 ratio of 8 and high space velocities of 1.5×10^5 h^{-1} GHSV which has demonstrated these catalyst achieved at high

pressures and high space velocities too [19].

In this work, applying of NaCl-MnO_x/SiO_2 as a catalyst for OCM reaction was studied. Its catalytic performance and the role of each catalyst component towards OCM were investigated. Optimal conditions of the process and the catalyst preparation; i.e. operating temperature, weight hourly space velocity (WHSV), molar feed ratio, and ratio of SiO_2 to NaCl-MnO_x; were determined using experimental and/or computational program to achieved high ethylene production as show in C_{2+} selectivity/yield and ethylene to ethane ratio and also low CO_x production.

2 Experimental Methodology

2.1 *Catalyst preparation and characterization*

NaCl-MnO_x/SiO_2 was synthesized using slurry mixed route method [20]. NaCl 64% by molar (99.9%, Ajax Finechem) was dissolved in distilled water, together with Mn $(NO_3)_2 \cdot 4H_2O$ (97%, Panreac) and SiO_2 nanoparticles (98%, Ajax Finechem) at the selected ratios of MnO_x to SiO_2 of 2:1, 1:1 and 4:1. The mixed solution was added to 50 mL of a complexing agent, NH_3 solution (30%, Panreac) and allowed to stir at room temperature until the solution was homogeneous. And the solution was then heated up to 95°C. The residual was dried in a vacuum oven at 110°C overnight and pre-calcined at 400°C for 9 h. The synthesized NaCl-MnO_x/SiO_2 catalyst was crushed and then sieved to 75–180 μm. After that, it was calcined in situ at 700°C in packed-bed reactor for 2 h to obtain NaCl-MnO_x/SiO_2 powder.

2.2 *Experimental set-up*

A 2 g NaCl-MnO_x/SiO_2 was packed in a quartz tubular reactor (i.d.=10 mm, o.d.=13 mm, length = 50 cm). The reactor was placed in the middle of an electric furnace (Inconel, 10 cm heating zone) where the bed's temperature was measured using a K-type thermocouple. Figure 1 illustrates rig's configuration. A mixture of CH_4 (40% CH_4/Ar, BIG Company), O_2 (40% O_2/Ar, BIG Company) and Ar (99.995%, BIG Company) were fed into the system using mass flow controllers (Brooks instrument flow, 0–220 mL/min). Argon was used as a make-up gas to adjust the total volumetric flow rate. The gaseous products; CH_4,
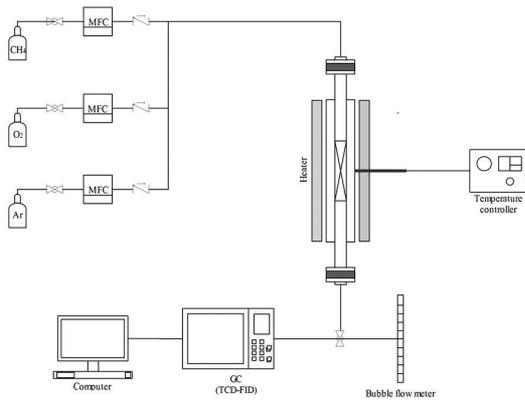
Figure 1: Schematic diagram of OCM experimental setup.

O$_2$, CO, CO$_2$, C$_2$H$_4$ and C$_2$H$_6$; were analyzed using on-line gas chromatography (Shimadzu GC-2014, FID-TCD detector) coupled with a Porapak Q capillary column.

Experimental results were demonstrated in terms of %conversion, %yield, %product selectivity which were calculated as shown in Equations (5)–(10).

$$CH_4\ conversion(\%) = \frac{mole\ of\ CH_4\ consumed}{mole\ of\ CH_4\ in\ the\ feed} \times 100\% \quad (5)$$

$$C_{2+}\ selectivity(\%) = \frac{mole\ of\ C_{2+}\ hydrocarbon}{total\ mole\ of\ carbon\ in\ the\ product} \times 100\% \quad (6)$$

$$CO\ selectivity(\%) = \frac{mole\ of\ CO\ hydrocarbon}{total\ mole\ of\ carbon\ in\ the\ product} \times 100\% \quad (7)$$

$$CO_2\ selectivity(\%) = \frac{mole\ of\ CO_2\ hydrocarbon}{total\ mole\ of\ carbon\ in\ the\ product} \times 100\% \quad (8)$$

$$C_{2+}\ yield(\%) = \frac{CH_4\ conversion\ \times\ C_{2+}\ selectivity}{100} \quad (9)$$

$$C_2H_4\ /\ C_2H_6\ (mol/mol) = \frac{moles\ of\ C_2H_4}{moles\ of\ C_2H_6} \quad (10)$$

2.3 *Computational analysis using Aspen plus*

Equilibrium concentration of each compounds were computationally calculated at each temperature in the range of 700–850°C under atmospheric by using Aspen Plus program to validate the efficiency of experimental results. OCM Reaction Network Presented by Stansch *et al.* were used for this simulation [21], [22]. The OCM process consists of nine heterogeneous and one homogeneous reaction steps as shown in Equations (1)–(4), (11), (16), (20), (22)–(25). An initial composition of 4 to 1 of methane/oxygen balanced with argon was used in equilibrium reactor.

Oxidative coupling methane (OCM)

$$2CH_4 + 2O_2 \rightarrow C_2H_4 + 2H_2O \quad \Delta H^o_{298} = -281\ kJ/mol \quad (11)$$

Methane partial oxidation (POM)

$$CH_4 + 0.5O_2 \rightarrow CO + 2H_2 \qquad \Delta H^o_{298} = -36\ kJ/mol \quad (12)$$

C$_2$ partial oxidation

$$C_2H_6 + O_2 \rightarrow CO + 3H_2 \qquad \Delta H^o_{298} = -137\ kJ/mol \quad (13)$$

Methane combustion

$$CH_4 + 2O_2 \rightarrow CO_2 + 2H_2O \qquad \Delta H^o_{298} = -802\ kJ/mol \quad (14)$$

$$CH_4 + 1.5O_2 \rightarrow CO + 2H_2O \qquad \Delta H^o_{298} = -519\ kJ/mol \quad (15)$$
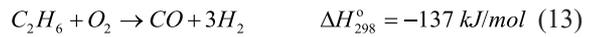
Combustion hydrocarbons

$$CH_4 + O_2 \rightarrow CO + H_2O + H_2 \quad \Delta H^o_{298} = -278\ kJ/mol \quad (16)$$

$$C_2H_6 + \frac{7}{2}O_2 \rightarrow 2CO_2 + 3H_2O \quad \Delta H^o_{298} = -1429\ kJ/mol \quad (17)$$

$$C_2H_6 + \frac{5}{2}O_2 \rightarrow 2CO + 3H_2O \quad \Delta H^o_{298} = -757\ kJ/mol \quad (18)$$

$$C_2H_4 + 3O_2 \rightarrow 2CO_2 + 2H_2O \quad \Delta H^o_{298} = -1323\ kJ/mol \quad (19)$$

$$C_2H_4 + 2O_2 \rightarrow 2CO + 2H_2O \quad \Delta H^o_{298} = -752\ kJ/mol \quad (20)$$
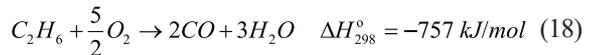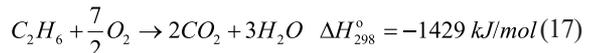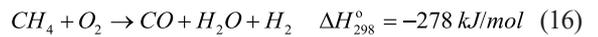
Steam reforming reaction

$$CH_4 + 2H_2O \rightarrow CO + 3H_2 \qquad \Delta H^o_{298} = -200\ kJ/mol \quad (21)$$

$$C_2H_4 + 2H_2O \rightarrow 2CO + 4H_2 \qquad \Delta H^o_{298} = +210\ kJ/mol \quad (22)$$
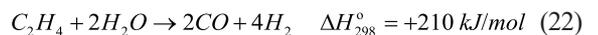
Hydrocarbon cracking reaction

$$C_2H_6 \rightarrow C_2H_4 + H_2 \qquad \Delta H^o_{298} = +136\ kJ/mol \quad (23)$$

Water gas shift reaction

$$CO + H_2O \rightarrow CO_2 + H_2 \qquad \Delta H^\circ_{298} = -41\,kJ/mol \quad (24)$$

$$CO_2 + H_2 \rightarrow CO + H_2O \qquad \Delta H^\circ_{298} = +41\,kJ/mol \quad (25)$$

CO oxidation reaction

$$CO + 0.5O_2 \rightarrow CO_2 \qquad \Delta H^\circ_{298} = -283\,kJ/mol \quad (26)$$

Coke formation, carbon cracking

$$CH_4 \rightarrow C + 2H_2 \qquad \Delta H^\circ_{298} = 75\,kJ/mol \quad (27)$$

$$C_2H_4 \rightarrow 2C + 2H_2 \qquad \Delta H^\circ_{298} = -52\,kJ/mol \quad (28)$$

$$C_2H_4 \rightarrow C + CH_4 \qquad \Delta H^\circ_{298} = 127\,kJ/mol \quad (29)$$

$$C_2H_6 \rightarrow 2C + 3H_2 \qquad \Delta H^\circ_{298} = 85\,kJ/mol \quad (30)$$

Boudouard reaction

$$CO_2 + C \rightarrow 2CO \qquad \Delta H^\circ_{298} = 127\,kJ/mol \quad (31)$$

3 Results and Discussion

3.1 *Diffractograms of NaCl-MnO$_x$/SiO$_2$*

Representative samples of fresh catalyst obtained from two different calcination temperatures at 400°C and after in situ calcined at 700°C for 2 h were examined by X-ray diffraction (XRD). Figure 2(a) shows the XRD pattern obtained after 400°C calcination for 9 h of the NaCl-MnO$_x$/SiO$_2$. The material showed 1) NaCl phase structure where its diffraction peaks were presented at 2θ= 27.33° 45.39° 53.82° 56.42° 66.17° and 75.24°. Manganese phase was found at 32.96°. Broad peak observed in the range of 20–25° indicating that silica oxide is amorphous phase [23]. Figure 2(b) shows the sharp peak of SiO$_2$ cristobalite at 21.91° and small peaks at 28.37° and 36.07° which is form after in situ calcined at 700°C for 2 h. It correspond to the formation of highly crystalline SiO$_2$ cristobalite due to the addition of NaCl could induce phase transformation at lower temperature [14]. Another phase of SiO$_2$ was observed at 20.81° 26.6° 36.5° 50.08° 59.94° and 68.06°, which corresponds to α-SiO$_2$. Both SiO$_2$ cristobalite and α-SiO$_2$ is highly
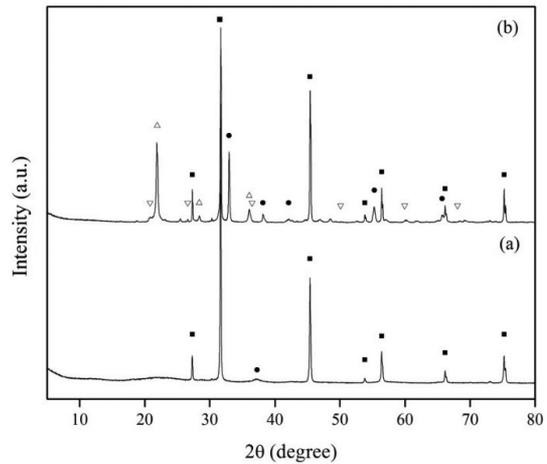
Figure 2: X-ray diffraction patterns of NaCl-MnO$_x$/ SiO$_2$ (2:1) at (a) 400°C and (b) 750°C calcination temperature. The (■), (●), (▽), and (△) symbols correspond to the peaks of NaCl, Mn7O$_8$SiO$_4$, α-SiO$_2$ and SiO$_2$ cristobalite, respectively.

selective catalysts [15], [24]. And Mn7O8SiO$_2$ was observed at 32.96° 38.15° 42.1° 55.27° and 65.7°. No other additional peaks was observed, indicating that NaCl-MnO$_x$/SiO$_2$ was successfully prepared using the slurry mixed route.

3.2 *Catalyst performance*

3.1.1 Effect of reaction temperature

The effect of reaction temperatures was studied from 700 to 850°C on 1) CH$_4$ and O$_2$ conversion, 2) selectivity of C$_{2+}$, CO and CO$_2$, and 3) yield of C$_{2+}$. It obtained from computational results and experimental results by homogeneous reaction and heterogeneous reaction. NaCl-MnO$_x$/SiO$_2$ (64%NaCl, ratio of MnO$_x$:SiO$_2$ = 2:1) was tested at WHSV of 3000 mL/g.h and feed ratio (CH$_4$ to O$_2$) of 4 to 1. From Figure 3(a) shows CH$_4$ conversion and O$_2$ conversion as a function of temperature, the results demonstrate that near-complete conversion of O$_2$ can be obtained whereas 47–50% CH$_4$ conversion from model, 0–3% from non-catalytic and 27–38% from experiments with using NaCl-MnO$_x$/SiO$_2$ as catalyst were achieved. This indicated that O$_2$ was the limiting reactant which can react in many pathways, including mainly associated reactions as methane partial oxidation [Equation (12)]

and complete methane combustion [Equations (14) and (15)], were also involved in the OCM process [25]. Theoretically, no production of C_{2+} was predicted, shown in Figure 3(b) and (c) for the results obtained from computer simulation. CO formation was expected at 100% selectivity, indicating that the overall OCM reaction mainly occurred via methane partial oxidation pathway in theory. Small amount of CO_2 formation, at low temperature lower than 700°C, was also suggested by the computational analysis. This result is corresponding to non-catalytic reaction but CO_2 formation was not detected.

However, the experimental results with using NaCl-MnO$_x$/SiO$_2$ shown in Figure 3(b) and (c) showed the opposite result, as C_{2+} production was observed at all temperatures. The maximum productivity was obtained at 750°C where yield and selectivity of C_{2+} were reported at 23% and 61%, respectively. CO selectivity was increased when the temperature increased due to its endothermicity ($\Delta H = +210$ kJ/mol) [Equation (22)] [26]. CO_2 selectivity was the highest at 700°C as it was a by-product of full combustion ($\Delta H = -802$ kJ/mol) [Equation (14)] [24], [27], which is well-known to occur at temperature ranging from 450 up to 1000°C [27]–[29]. The OCM process was then concluded to be a highly selective reaction and unlikely to occur without a catalyst [30]. From the experimental results, C_{2+} production was encouraged by NaCl-MnO$_x$/SiO$_2$ catalyst due to its effective alkali and transition metals. NaCl offered great performance on the selective formation of ethylene and also suppressed CO formation [11], [31]–[34]. C_{2+} productivity was increased when the temperature increased from 700 to 750°C, although decreased when the temperatures were higher than 750°C because of an involvement of C_{2+} cracking/steam reforming, and also the deactivation of catalyst in such temperature range [35]–[37]. At this temperature range, the steam reforming [Equation (21)], reverse water gas shift [Equation (25)], and combustion of hydrocarbons [Equations (16)–(20)] led to the rise in CO and CO_2 formation and were also involved as reported earlier in many previous works [36]–[38]. Carbon cracking [Equations (27)–(30)] occurred coke accumulation and affect catalyst deactivation [36]. In addition, thermal deactivation of the catalyst is occurred from melting of sodium chloride (the melting point of sodium chloride is approximately 800°C) which is very important factor
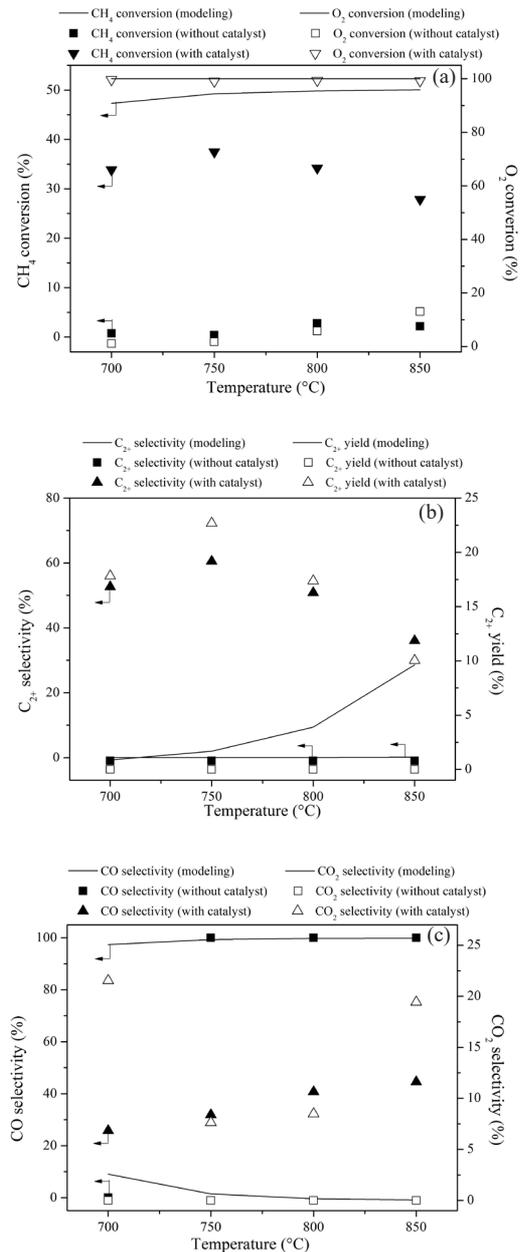
Figure 3: Comparison of results between reaction's activities achieved a) methane conversion and oxygen conversion b) C_{2+} selectivity and C_{2+} yield and c) CO selectivity and CO_2 selectivity via model and experiment (without catalyst and with catalyst ratio of NaCl-MnO$_x$:SiO$_2$ = 2:1) under WHSV of 3000 mL/g.h and feed ratio (CH_4 to O_2) of 4 to 1 in the reaction temperature range from 700 to 850°C.
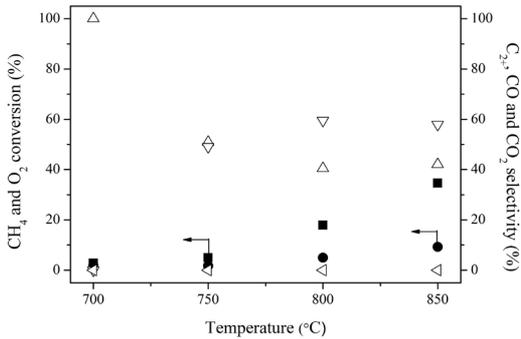
Figure 4: The effect of NaCl to CH_4 conversion (●), O_2 conversion (■), C_{2+} selectivity (△), CO selectivity (▽), and CO_2 selectivity (◁) at WHSV of 3000 mL/g.hr and feed ratio (CH_4 to O_2) of 4 to 1 in the reaction temperature range from 700 to 850°C.

Figure 5: The effect of MnO_x to CH_4 conversion (●), O_2 conversion (■), C_{2+} selectivity (△), CO selectivity (▽), and CO_2 selectivity (◁) at WHSV of 3000 mL/g.h and feed ratio (CH_4 to O_2) of 4 to 1 in the reaction temperature range from 700 to 850°C.

for C_{2+} productivity [39]. The loss of NaCl is started to melting, water vapor reacted with sodium chloride to form hydrogen chloride and sodium hydroxide in the product stream [40]. The operating temperature lower than 800°C is therefore suitable for the use of NaCl-MnO_x/SiO_2 in OCM process.

3.1.2 The role of NaCl, MnO_x, and SiO_2 in the NaCl-MnO_x/SiO_2 on catalytic performance

NaCl, MnO_x, and SiO_2 in the NaCl-MnO_x/SiO_2 was investigated as a function of temperature ranging from 700–850°C at WHSV of 3000 mL/g.h and feed ratio (CH_4 to O_2) of 4 to 1 in terms of 1) CH_4 and O_2 conversion and 2) selectivity of C_{2+}, CO and CO_2.

Figure 4 shows the results of NaCl performance. It demonstrates that NaCl affected to both CH_4 conversion, which increased from 1.75% at 700°C to 9.25% at 850°C, and O_2 conversion, which increased from 2.80% at 700°C to 34.64% at 850°C. However, C_{2+} selectivity decreased when temperature was raised due to C_{2+} cracking and partial oxidation reaction [Equations (15), (26), (31)] [35], [36]. And also CO selectivity increased with increasing temperature due to partial oxidation of methane and C_{2+} reaction [Equations (12) and (13)]. CO_2 was not detected at all temperatures indicated that full combustion reaction was not occurred. Therefore, NaCl is suggested to play an important role as active site for C_{2+} productivity [33]. Meanwhile, it inhibited the CO_2 formation, which is in agreement with other researchers [11], [39]–[41].

MnO_x catalyst showed complete conversion of O_2, while the conversion of CH_4 was approximately at 10% all reaction temperatures studied in this work as shown in Figure 5. MnO_x could adsorb oxygen on the surface of catalyst to be surface-active oxygen by transferring electron from the surface of catalyst to oxygen molecule due to good electrical conductivity property and low energy gap [14], [42]. Mostly methane reacted with surface-active oxygen via complete methane combustion, evidenced by high CO_2 production for all temperatures. At high temperature, CO_2 formation slightly decreased due to an increase of CO selectivity by Boudouard reaction [Equation (31)] [43], [44]. Moreover, increasing of CO selectivity occurred partial oxidation of methane. Therefore, MnO_x provided large amount of surface-active oxygen which represents an increasing of the surface lattice oxygen mobility is increased but it affected to lower C_{2+} production [14], [34].

Figure 6 showed the results of SiO_2 support catalyst for the OCM. Maximum O_2 conversion (99.6%) and CH_4 conversion (15%) were occurred at the highest temperature. The difference between the results of SiO_2 and homogeneous reaction demonstrated that SiO_2 affect C_{2+} formation due to the OCM pathway [45]. Methane partial oxidation occurred which can be seen from almost 100% CO selectivity at 700°C. Decreasing of CO caused by the reduction of methane concentration due to methane cracking over than 700°C [46]. It demonstrates that the ratio of methane to oxygen decreased to occur complete methane combustion as seen from the increase of carbon dioxide selectivity,
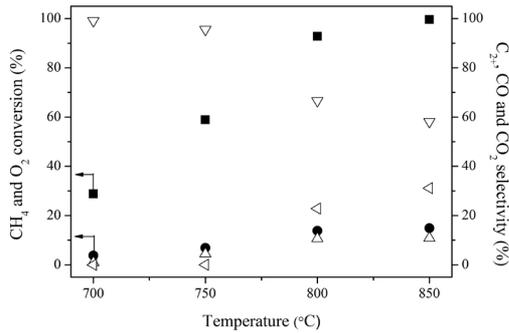
Figure 6: The effect of SiO_2 to CH_4 conversion (●), O_2 conversion (■), C_{2+} selectivity (△), CO selectivity (▽), and CO_2 selectivity (◁) at WHSV of 3000 mL/g. hr and feed ratio (CH_4 to O_2) of 4 to 1 in the reaction temperature range from 700 to 850°C.

oxygen conversion and methane conversion. Thereby, SiO_2 based catalyst is considered to play a vital role for C_{2+} productivity and the consumption of methane and oxygen.

3.1.3 Effect of Weight hourly space velocity (WHSV)

2 grams of NaCl-MnO_x/SiO_2 was used in the following experiments by vary total inlet flow rates, all carried out at 750°C. Ratio of CH_4 to O_2 was fixed at 4. The effect of WHSV was varied in range 1500–6000 mL/g.h at 1500, 2250, 3000, 3750, 4500, and 6000 mL/g.h. The experiments were carried out at fixed reaction temperature of 750°C and mole ratio of CH_4 to O_2 at 4.

Figure 7 presents the influence of WHSV on CH_4 conversion, C_{2+} and CO_x selectivity, C_2 yield and C_2H_4/C_2H_6 mole ratio. At 6000 mL g^{-1} h^{-1}, it was found that methane conversion and C_{2+} product were low due to short contact time. Mostly methane flowed through catalyst without reacting but some part of methane was consumed, resulted in undesired product CO_x. Increasing of residence time caused an increase of methane conversion and C_{2+} selectivity but lower CO_x selectivity. It was supported one of the assumption that CO_x formation depends on the residence time of reaction. The homogeneous reaction in the gas phase might occur when the residence time in the catalyst bed is too short [25]. Ratio of ethylene to ethane increased with decreasing of WHSV indicated that ethylene formation occurred via continually reaction. At a longer residence time (low WHSV), the remaining
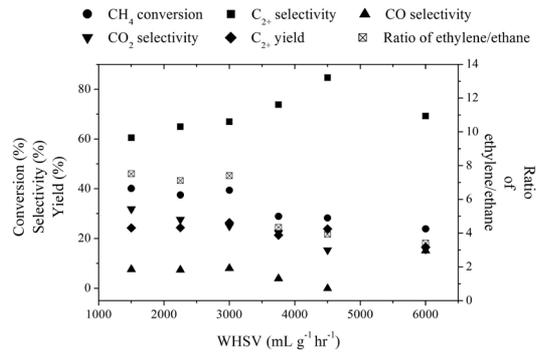
Figure 7: Methane conversion (●), C_{2+} selectivity (■), CO selectivity (▲), CO_2 selectivity (▼), C_{2+} yield (►) and C_2H_4/C_2H_6 ratio (⊠) with catalyst ratio of NaCl-MnO_x:SiO_2 = 2:1 under different WHSV with a reaction temperature at 750°C in ratio of methane and oxygen is 4.
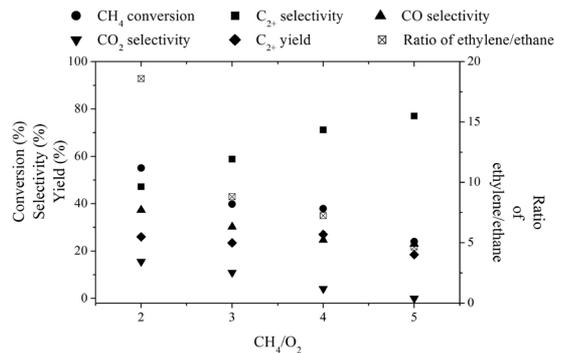
Figure 8: Methane conversion (●), C_{2+} selectivity (■), CO selectivity (▲), CO_2 selectivity (▼), C_{2+} yield (◆) and C_2H_4/C_2H_6 ratio (⊠) with catalyst ratio of NaCl-MnO_x:SiO_2 = 2:1 under different inlet molar ratio of methane and oxygen with a reaction temperature at 750°C in WHSV of 3000 mL g^{-1} h^{-1}.

oxygen in the reactor formed nonselective products as CO_x. It demonstrated that ethylene and ethane are an intermediate components [15], [37], [47]. The best performance was observed that C_{2+} yield (27%) and molar ratio of C_2H_4/C_2H_6 (7.2) obtained when the WHSV was at 3000 mL g^{-1} h^{-1}.

3.1.4 Effect of feed ratio

The effect of CH_4 to O_2 feed ratio was studied in the range from 2 to 5 at reaction temperature of 750°C. Figure 8 showed the effect of the feed ratio on catalytic
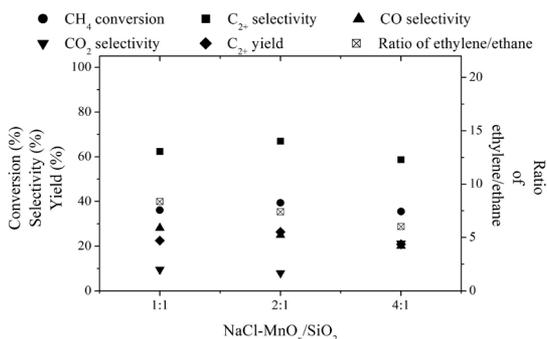
Figure 9: Methane conversion (●), C_{2+} selectivity (■), CO selectivity (▲), CO_2 selectivity (▼), C_{2+} yield (►) and C_2H_4/C_2H_6 ratio (⊠) under different NaCl-MnO_x:SiO_2 ratio in 3000 mL/g.hr WHSV and CH_4/O_2 ratio is 4 at 750°C of reaction temperature.

Figure 10: Methane conversion (■), C_{2+} selectivity (▲), and C_{2+} yield (●) with catalyst ratio of NaCl-MnO_x:SiO_2 = 2:1 in 3000 mL/g.h WHSV and CH_4/O_2 ratio is 4 at 750°C of reaction temperature.

performance of the NaCl-MnO_x/SiO_2 towards OCM reaction. CH_4 conversion was observed to decrease with increasing ratio of methane and oxygen whereas the C_{2+} selectivity increased when CH_4/O_2 ratio was increased. CO and CO_2 selectivity decreases with increasing CH_4/O_2 ratio, which affects oxidation of CO, and CO_2. This result is in good agreement with the work reported by Farrell *et al.* [21], of which reported the decrease of CH_4/O_2 molar ratio led to an increase of CO and CO_2 production. When the methane was fed excess, the reaction pathway is likely toward the production of C_2. Appropriate ratio of methane to oxygen for achieved 25% C_{2+} yield is at 4.

3.1.5 Effect of NaCl-MnO_x to SiO_2 molar ratio

The amount of active site NaCl-MnO_x was investigated for the effect to OCM process performance was investigated by varying NaCl-MnO_x to SiO_2 mole ratio at 1:1, 1:2, and 1:4.

The results in Figure 9 demonstrated that the amount of active site affect process performance. It has been seen that the activity of catalyst and product selectivity were increased when increasing of NaCl-MnO_x (active site) and it also caused CO_x is decreased. It was following the OCM mechanisms that oxygen adsorption on the catalyst surface. Hydrogen abstraction from methane occur on the catalyst surface to form methyl radicals. Ethane formation was occurred from couple methyl radicals.

Then dehydrogenation reaction was occurred to form ethylene [22], [26], [48]. At active site to support ratio of 4, methane conversion and C_{2+} selectivity were decreased due to less area of support that make poor distribution of the active site and also the unification of active site without support decreased the surface reaction causing C_{2+} yield to decreased [45]. At 2:1 of NaCl-MnO_x to SiO_2 achieved the methane conversion, C_{2+} selectivity and C_{2+} yield at 750°C about 39, 66 and 26%, respectively.

3.1.6 Catalyst stability

Figure 10 shows NaCl-MnO_x/SiO_2 catalyst was stable throughout a 12 h run at 750°C, 3000 mL/g.h WHSV and CH_4/O_2 ratio is 4.

The CH_4 conversion was stabilized at about $38 \pm 3.4\%$ and the best C_{2+} selectivity reached $72 \pm 1.6\%$. C_{2+} yield maintained at $27 \pm 1.2\%$ during 12 h period continuous reaction without recharging the catalyst. The optimum condition can stabilized the performance of NaCl-MnO_x/SiO_2.

Table 1 was summarized performances of the process for different catalysts in terms of reactant conversion and product selectivity under OCM reaction. NaCl-MnO_x/SiO_2 developed in our work shows superior catalytic properties as it could be operated at low temperature to achieve high performance as C_{2+} yield, and ethylene to ethane about 7.2 at optimum conditions.

Table 1: Catalytic performance for oxidative coupling of methane over various catalysts

Catalyst	Operating Condition	CH_4 Conversion	C_{2+} Yield	C_{2+} Selectivity	C_2H_4/C_2H_6	Ref.
Na-CaO	T = 750°C, CH_4/O_2 = 4	24.7	17	68.8	1.2	[47]
K-CaO	WHSV = 5140 $cm^3 \cdot g^{-1} \cdot h^{-1}$	25.2	14.8	58.9	1.2	
Mn/Na_2WO_4/SiO_2	T = 775°C, CH_4/air = 7.5	20	16	80	1.4	[14]
Li-TbO_x/n-MgO	T = 700°C CH_4/O_2 = 4	24.9	14.5	63.6	1.4	[49]
Li- Sm_2O_3/n-MgO	GHSV = 2400 h^{-1}	24.4	13.2	62.5	1.7	
Ce-Mn- Na_2WO_4/SiO_2	T = 800°C, CH_4/air = 1	21	-	84	-	[48]
Mn-Na_2WO_4/SiO_2	T = 800°C, CH_4/air = 2	45.4	19.5	41.4	-	[50]
Mn– Na_2WO_4/SiO_2	T = 825°C, CH_4/O_2 = 2.5	35.4	20.6	58.1	2.75	[51]
Mn– Na_2WO_4/n-SiO_2	T = 800°C, CH_4/O_2 = 4	25.2	18.5	73.3	1.7	[24]
MnxOy–Na_2WO_4/SiO_2-rutile	T = 750°C, CH_4/O_2 = 4	6.5	3.5	58.6	-	[52]
MnxOy–Na_2WO_4/SBA-15	T = 750°C	13	-	68	-	[53]
NaCl-MnO_x/SiO_2	T = 750°C CH_4/O_2 = 4 WHSV = 3000 $cm^3 \cdot g^{-1} \cdot h^{-1}$	38	27	71.2	7.24	Our work

4 Conclusions

The developed NaCl-MnO_x/SiO_2 catalyst, which was synthesized by using slurry mixed method, showed a good performance for OCM reaction as thermodynamic limitation could be overcome. C_{2+} selectivity could be increased by NaCl and SiO_2 whereas MnO_x and SiO_2 improved conversion of methane and oxygen. Key process parameters, including reaction temperature, WHSV, CH_4 to O_2 feed ratio, NaCl-MnO_x to SiO_2 molar ratio, were investigated. Increasing reaction temperature to lower than 800°C was found to render methane conversion, C_{2+} selectivity and ethylene and ethane ratio. The increment of WHSV, which represents low residence time in the reactor, was found to decrease methane conversion, C_{2+} yield and ratio of ethylene to ethane. An increase of methane/oxygen ratio led to lower conversion because the demand of methane in the reaction consumed less than the amount of inlet methane. The increase of active site to support ratio offered good catalytic activity; however, an excess of active site could cause active site to aggregate. Our investigation suggested that the NaCl-MnO_x/SiO_2 catalyst exhibits excellent and stability performance for the OCM reaction. High methane conversion, C_{2+} selectivity, C_{2+} yield and C_2H_4/C_2H_6 ratio about 38%, 71%, 27% and 7.2, respectively, could be obtained with using NaCl-MnO_x/SiO_2 catalyst, which was calcined at 400°C, WHSV at 3000 mL g^{-1} h^{-1}, the ratio of methane/oxygen at 4, active site/support of catalyst at 2 and operating temperature at 750°C. These experiment is the highest value reported so far to the best of our knowledge.

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